#### ANDREAS LENDLEIN

## **16.1 Introduction**

The introduction of resorbable, synthetic suture materials represented important progress in surgery in the early 1970s. Those sutures consisted of  $poly(\alpha-hydroxyacid)$ s like polyglycolide and the copolyesters of  $L, L$ -dilactide and diglycolide.<sup>1,2</sup> Originally commercialized by American Cyanamid, Ethion Inc. and Davis  $\&$  Geck, these aliphatic polyesters have been successfully applied until today and have become a well-accepted standard. Due to the time-consuming and cost-intensive process for the approval of novel biomedical devices by federal administration, only a few further biodegradable polymers have reached the market since then. Polyanhydrides are an example of a group of materials which has been introduced to clinics during the 1980s.<sup>3</sup> Based on a polyanhydride matrix, implantable drug delivery systems like Gliadel (Guilford Pharmaceutical Co., Baltimore) and Septicin<sup>TM</sup> (Abbott Laboratories, Illinois) have been developed. Gliadel<sup>TM</sup> is applied for the treatment of brain cancer (glioblastoma multiforme). Gliadel<sup>TM</sup> pellets are used to fill cavities caused by surgical treatment of brain tumours and in addition to combat remaining tumour cells. With Septicin<sup>TM</sup> implants, it is possible to cure chronic bone infections.

To be degradable, a biomaterial needs bonds which are cleavable under physiological conditions. In the case of the aliphatic polyesters mentioned above, as well as the polyanhydrides, these are hydrolysable bonds. There are two mechanisms for hydrolytic degradation *—* bulk degradation and surface erosion.<sup>1</sup> Both mechanisms differ in the ratio between the rate of diffusion of water in the polymer matrix and the rate of hydrolysis of the cleavable bond. If the rate of diffusion is higher than the rate of hydrolysis, a water uptake of a few per cent, typically 1–3 wt.%, can be observed. The hydrolysable bonds within the bulk will be degraded almost homogeneously. This mechanism is called bulk degradation. For hydrophobic polymers, the rate of diffusion of water into the polymer matrix can be significantly lower than the rate of



16.1 General schematic representation of the degradation behaviour of degradable polymers: (a) bulk degradation, (b) surface erosion.

cleavage of the hydrolysable bonds. Here the degradation is taking place only within a thin surface layer of the implant. In the case of surface erosion the degradation rate therefore depends on the surface area of a device. While polyanhydrides showsurface erosion, polyhydroxyacids undergo bulk degradation. A general scheme of the degradation behaviour for both mechanisms is given in Fig. 16.1.

The number of potential applications for biodegradable implant materials is increasing constantly. One reason can be seen in the growing confidence of clinicians in the concept of degradable biomaterials based on the successful application of the established polymers. Another motivation can be found in completely new therapeutic methods, which have been developed taking advantage of the concept of biodegradable polymers such as tissue engineering.<sup>4,5</sup> Tissue engineering is an interdisciplinary approach aiming at the generation of newfunctional living tissue, which can be transplanted into a patient in terms of reconstructive surgery. This newtissue should be fabricated using living cells associated to a degradable porous scaffold. The scaffold should determine the three-dimensional shape of the resulting tissue, and should be degraded while the cells are growing and replacing the artificial structures.

The requirements for an implant material are determined by the respective application. The key properties of degradable biomaterials are their mechanical properties, degradation rate and behaviour, their functionality and their biocompatibility. For each application, a specific set of the properties mentioned is needed. With the growing number of potential applications, the number of required materials with specific combinations of properties is also increasing. As the variability of properties is limited for those

biomaterials established, a newgeneration of biodegradable implant materials is demanded.

In the following section, promising candidates for the next generation of degradable biomaterials will be introduced. This class of biomaterials allows variation of macroscopic properties within a wide range by only small changes in the chemical structure. As an additional functionality, these newmaterials showshape memory properties.

## **16.2 Fundamental aspects of shape memory materials**

Shape memory materials are able to memorize a second, permanent shape besides their actual, temporary shape. After application of an external stimulus, e.g. an increase in temperature, such a material can be transferred into its memorized, permanent shape. The process of programming and restoring a shape can be repeated several times. This behaviour is called the thermally induced 'one-way' shape memory effect.

The shape memory effect has been reported for different materials, such as metallic alloys, <sup>6-10</sup> ceramics, <sup>11,12</sup> and glasses<sup>11</sup>, polymers<sup>18-30</sup> and gels<sup>13-17</sup>.

Shape memory alloys (e.g. CuZnAl-, FeNiAl-, TiNi-alloys) are already being used in biomedicine as cardiovascular stents, guidewires and orthodontic wires. The shape memory effect of these materials is based on a martensitic phase transformation.

Several types of shape memory gels are described in the literature.<sup>13-17</sup> Two different concepts are explained below. In the first system the shape memory effect is 'one-way' and originates from the chemical structure of the polymer network. The other system is an example of a reversible 'two-way' shape memory effect. However, this effect is being achieved by the design of the gel specimen as a bilayer system.

The first system can be prepared by a radical copolymerization of stearyl acrylate and acrylic acid with *N*,*N*-methylenebisacrylamide as a crosslinker. Due to the intermolecular aggregation of the stearyl acrylate side chains, a crystalline lamellar structure can be observed in the dry as well as the swollen state in DMSO at room temperature. The swelling ratio of a gel film grows with increasing temperature up to 47 °C corresponding to the melting point of the stearyl side chains. This crystallizable side chain is the physical cross-link which can be used to fix a temporary shape. The permanent shape is being determined by the covalent cross-links of the polymer network. In this way, a thermally induced one-way shape memory effect can be programmed.

A reversible shape memory effect can be achieved using modulated gel technology.<sup>14</sup> These gels consist of two components, typically in the form of layers. The first component is not sensitive to an external stimulus (substrate element), while the second part is responsive to a selected stimulus (control element). The design of the gel specimen is optimized in such a way that a small change of the control element causes a large movement of the substrate element. An example of such a system is a partially interpenetrating system. The non-responsive part consists of a polyacrylamide gel. The control element is an interpenetrating network of the same polyacrylamide gel with a crosslinked poly(*N*-isopropylacrylamide) (NIPA). It is a specific property of the ionic NIPA gel (containing a small amount of sodium acrylate) to drastically shrink at temperatures higher than 37 °C. Since this change in volume of the control component is reversible, the shape memory effect is also reversible.

The shape memory effect of polymers, e.g. heat-shrinkable films or tubes,<sup>18</sup> is not a specific bulk property, but results from the polymers' structure and morphology. The effect is persistent in many polymers, which might differ significantly in their chemical composition. However, only a few shape memory polymer systems have been described in the literature. One example is segmented polyurethanes.<sup>19-30</sup> The thermal transition, which triggers the shape memory effect, can be a glass transition<sup>21-26</sup> as well as a melting point.<sup>20-27</sup> Segmented polyurethanes have found some applications, e.g. as chokes in cars. However, they are not suitable as degradable biomaterials for two reasons. On the one hand, the urethane bonds of their hard segments are hardly hydrolysable. On the other hand, the degradation products would be highly toxic lowmolecular weight aromatic compounds.

### **16.3 Concept of biodegradable shape memory polymers**

Biodegradable, stimuli-sensitive polymers have great potential in minimal invasive surgery. Degradable implants can be brought into the body through a small incision in a compressed or stretched temporary shape. Upon heating up to body temperature, they switch back to their memorized shape. Repeat surgery for the removal of the implant is not required, since the materials will degrade after a predetermined implantation time period.

Structural concepts for tissue-compatible and biodegradable polymers, thermoplastic elastomers,  $31$  and thermosets  $32$  with shape memory capabilities will be introduced. Their thermal and mechanical properties and degradation behaviour will be explained. An important precondition for the shape memory effect of polymers is elasticity. An elastic polymeric material consists of flexible segments, so-called network chains, which are connected via netpoints or junctions. The permanent shape of such a polymer is determined by the netpoints. The network chains take a coil-like conformation in unloaded condition. If the polymer is stretched, the network chains become extended



16.2 General schematic representation of the shape memory effect.

and oriented. In the case of an ideal entropy elastic material, the original shape is recovered after the stress is released.

An elastic polymer gains a shape memory functionality if the deformation of the material can be stabilized in the temperature range which is assigned for the specific application. This can be realized by using the network chains as a kind of molecular switch. For this purpose it should be possible to vary the segment flexibility as a function of temperature. Ideally, this process should be reversible. One way to obtain a switch functionality is given by the introduction of a thermal transition of the network chains at a temperature  $T_{\text{trans}}$ . Above  $T_{\text{trans}}$ , the segments are flexible, while below the transition temperature, the flexibility of the network chains can be limited to a certain extent. Below a glass transition temperature  $T_{\rm g}$ , the flexibility of the network is frozen. If the thermal transition is a melting point, the network may become partially crystalline at temperatures below the melting temperature  $T<sub>m</sub>$ . The so-formed crystalline domains prevent the segment chains from spontaneously recovering a coil-like conformation. The process of programming a temporary shape and the recovery of a permanent shape is shown in Fig. 16.2. Above  $T_{\text{trans}}$ , the segments are flexible and the polymer can be deformed elastically. The programmed shape is fixed by cooling the material to a temperature below  $T_{\text{trans}}$ . Upon heating above  $T_{\text{trans}}$ , the permanent shape can be recovered.

For biomedical applications, a thermal transition of the segment chains in the range between room and body temperature is of great interest. Suitable segments for degradable shape memory polymers can be found by regarding



16.3 Dependence of thermal transition on molecular weight: (a) oligo[glycolide-co-(L-Kwsir-lactide)]diol having a glycolate content of 15 mol %, (b) oligo( $\varepsilon$ -caprolactone)diol.

the thermal properties of well-established degradable biomaterials. From this assortment, two promising candidates can be extracted:  $poly(\varepsilon$ -caprolactone), which has a  $T_m$  of 61 °C, and the amorphous copolyesters of diglycolide and dilactides, showing glass transition temperatures  $T<sub>e</sub>$  in the range from  $35^{\circ}$ C to  $55^{\circ}$ C. A fine-tuning of the respective thermal transition can be managed by variation of the molecular weight and the comonomer ratio (see Fig. 16.3).

Appropriate macrodiols are produced via ring opening polymerization of cyclic diesters or lactones initialized by lowmolecular weight diols (see Fig. 16.4).<sup>33</sup> The sequence structure of cooligomers can be influenced by application of a transesterification catalyst. The molecular weight of the oligomers can be controlled by the monomer/initiator ratio. Typically, the molecular masses Mn being obtained are between  $500 \text{ g mol}^{-1}$  and  $10000 \text{ g mol}^{-1}$ . The net points can either be of physical or chemical nature. In the case of physical crosslinks, e.g. crystallizable segments with  $T_{\rm m} \gg T_{\rm trans}$ , the resulting polymer represents a thermoplastic elastomer. These materials can be melt processed, e.g. by extrusion or mould injection. Here, the permanent shape can be changed several times. In contrast, the permanent shape of a covalently crosslinked polymer network cannot be changed after the crosslinking process.

Important characteristics to be adjusted are the mechanical properties of the polymers in their permanent and temporary shape, the thermal transition temperature*T*-, the rate and the mechanism of the degradation process, and the shape memory properties.



16.4 Synthesis of macrodiols via ring-opening polymerization of lactones or cyclic diesters.<sup>33</sup> Courtesy of Wiley-VCH.

### **16.4 Degradable thermoplastic elastomers having shape memory properties**

### 16.4.1 Synthesis

In order to synthesize biodegradable multiblock copolymers, the oligoesterdiols and cooligoester diols are linked by bifunctional junction units, e.g. diisocyanates, diacidchlorids or phosgene (see Fig. 16.5). High molecular weight polymers in the range of  $M_w = 100000 \text{ g mol}^{-1}$  need to be obtained in order to get the desired mechanical properties. The resulting thermoplastic copolyesterurethanes are tough and show high elongations at break  $\varepsilon_R$ . These linear multiblock copolymers are phase segregated and consist of crystallizable hard segments  $(T_m)$  and amorphous switching segments  $(T_{trans} = T_g)$ , e.g. poly[(L-lactide)-*co*glycolide] with a glycolate content of  $15 \text{ mol }$ %. The permanent shape of these materials is obtained by melting the polymer followed by cooling to a temperature  $T_{\rm m} > T > T_{\rm trans}$ . The shape memory polymer can now be brought



16.5 Synthesis of multiblock copolymers via polyaddition reaction. Courtesy of Wiley-VCH.

into its temporary shape, which is being fixed by cooling below  $T_{\text{trans}}$ . The permanent shape can be recovered by heating the material above  $T_{trans}$ .

## 16.4.2 Thermomechanical properties of thermoplastic elastomers

The shape memory effect can be determined quantitatively by cyclic thermo-mechanical tests. These measurements are performed in a tensile tester equipped with a thermo-chamber. At a temperature above  $T_{\text{trans}}$ , a bone-shaped sample is fixed between two clamps and stretched. If the maximum elongation has been reached, the sample is cooled down to a temperature below  $T_{\text{trans}}$ . The clamps then return to their initial distance. The sample reacts with bending. After reheating to a temperature above  $T_{\text{trans}}$  but below  $T_{\text{m}}$  of the hard segment, the next cycle can be started. Figure 16.6 shows an example for the result of such a cyclic thermomechanical test.

# 16.4.3 Degradability

As shown in Fig. 16.7, accelerated hydrolytic degradation experiments with different copolyester-urethanes in buffer solution of pH 7 at 70 °C showed that these materials are hydrolytically degradable. The degradation rate varies within a wide range. In contrast to the degradation behaviour of several polyhydroxyacids,mass loss of the investigated shape memory polymers starts early and shows linear behaviour during the whole degradation period.

# 16.4.4 Toxicity testing

In a first set of experiments, the multiblock-copolymers proved to be non-toxic. The CAM (chorioallantoic membrane) test is a sensitive test for cell toxicity. It is performed by placing a sterilized sample of the polymer on the



16.6 Cyclic thermomechanical testing of a polymer with an oligo[glycolide-co-(L-lactide)] as switching segment with  $T<sub>g</sub> = 35 °C$ ; hard segment content: 22 w/w %; (Cycles:  $n = 1$  ———;  $n = 2$  ------;  $n = 3$  ……;  $n = 4$  $--:$ ;  $n = 5$   $---$ .



 $\nabla$  PDC31;  $\odot$  PDC40;  $\triangle$  PDL30).

chorioallantoic membrane of a fertilized chicken egg for two days. After incubation, the growth of blood vessels around the polymer sample is observed. In case of a non-toxic polymer, the blood vessels remain unchanged and their development is not restricted. In case of incompatibility, the sample causes changes in the number and shape of blood vessels, and the formation of a thrombus might occur (see Fig. 16.8).



16.8 CAM test after 48 h incubation time: (a) multiblock copolymer, edge length of the sample 1–2mm, (b) control experiment: incompatible sample causes thrombus (dark spot).1 Courtesy of Wiley-VCH.



16.9 Synthesis of polymer networks with shape memory properties: (a) synthesis of the dimethyacrylate macromonomers, (b) cross-linking of the macromonomers.

### **16.5 Degradable polymer networks having shape memory properties**

Based on the same switching segments as mentioned for the thermoplastic elastomers, a group of shape memory polymer networks can be prepared. Instead of crystallizable hard segments, covalent cross-links are introduced. For this purpose, the macrodiols can be turned into macrodimethacrylates, which can be cross-linked by photocuring. An example for the synthesis of biodegradable shape memory polymer networks is shown in Fig. 16.9. A potential educt is poly( $\varepsilon$ -caprolactone) dimethacrylate with molecular weights between 1000 and 10 000. By copolymerization with *n*-butylacrylate, Abnetworks can be obtained.<sup>32</sup> The permanent shape of these polyester networks is fixed via photocuring. The thermo-mechanical properties of the network

can be tuned by the choice of the molecular weight of the respective macrodimethacrylates. The temporary shape can be formed by deformation of the sample under temporary heating above *T* .

## **16.6 Conclusion and outlook**

Biodegradable shape memory polymers are candidates for the next promising generation of implant materials. The fact that these materials belong to a polymer system allows the adjustment of certain properties in a wide range, e.g. mechanical properties and degradation behaviour. Today, such materials can be synthesized in a kilogram scale.

In contrast to metallic shape memory alloys like NiTi-alloys, the polymers presented here combine the features of degradability and high elasticities, with elongations at break up to 1500%. Furthermore, shape memory polymers can be programmed much faster, allowing the individual adaptation of an implant to the patient's needs during surgery. Compared to hydrogels, these materials exhibit much higher mechanical strength.

From the point of view of economy and costs in healthcare systems, biodegradable shape memory polymers have two major advantages. Implants based on these materials can be brought into the body by minimally invasive methods, e.g. belly button surgery, allowing more careful treatment of patients; in addition, repeat surgery for the removal of the implant can be circumvented. The high potential of shape memory polymers for biomedical applications will therefore have a decisive influence on the way in which medical devices are designed in the future.

# **Acknowledgements**

The author would like to thank Dr Steffen Kelch for his support in creating the manuscript for this chapter, as well as the author's research team, which has contributed to the experimental results being described. For financial support, the author is grateful to BMBF (BioFuture project no. 0311867) and Penguin-Foundation, as well as Fonds der Chemischen Industrie.

# **References**

- 1 Lendlein A, 'Polymere als Implantatmaterialien', *Chemie in unserer Zeit*, 1999, 33, 279*—*95.
- 2 Shalaby S W and Johnson R A, 'Synthetic absorbable polyesters'. In S W Shalaby (ed.), *Biomedical Polymers*, Hanser Publishers, München, 1994.
- 3 Laurencin C T, Sobrasua I E M and Langer R S, *Poly(anhydrides)*. In J O Hollinger

(ed.), *Biomedical Applications of Synthetic Biodegradable Polymers*, CRC Press, Boca Raton, 1995.

- 4 Bronzino J D,*The Biomedical Engineering Handbook*, CRC Press, Boca Raton, 1995.
- 5 Silver F H and Doillon Ch, *Biocompatibility*: *Interactions of Biological and Implantable Materials, VCH-Wiley, New York, 1989.*
- 6 Perkins J, *Shape Memory Effects in Alloys*, Plenum Press, NewYork, 1975.
- 7 Lipscomb P and Nokes L D M, *The Application of Shape Memory Alloys in Medicine*, MEP, Suffolk, 1996.
- 8 Linge L and Dahm S, 'Practical aspects of using 'super-elastic' archwires for edgewise technique', *Fortschr*. *Kieferorthop*., 1994, 55, 324*—*9.
- 9 Quandt E, Halene C, Holleck H, Feit K, Kohl M and Schlossmacher P, 'Sputter deposition of TiNi and TiNiPd films displaying the two-way shape memory effect', *The 8th International Conference on Solid*-*State Sensors*, *Actuators and Eurosensors* IX. Stockholm, 1995.
- 10 Cederström J and Van Humbeeck J, 'Relationship between shape memory material properties and applications', *Journal Phys*. *IV*, *Coll*. *C*2, *Suppl*. *J*. *Phys*. *III*, 1995, 5, 335*—*41.
- 11 Itok A, Miwa Y and Iguchi N, 'Shape memory phenomena of glass-ceramics and sintered ceramics', *J*. *Japan Inst*. *Metals*, 1990, 54, 117*—*24.
- 12 Swain M V, 'Shape memory behaviour in partially stabilized zirconia ceramics', *Nature*, 1986, 322, 234*—*6.
- 13 Osada Y and Matsuda A, 'Shape memory in hydrogels', *Nature*, 1995, 376, 219.
- 14 Hu Z, Zhang X and Li Y, 'Synthesis and application of modulated polymer gels', *Science*, 1995, 269, 525*—*7.
- 15 Kagami Y, Gong J P and Osada Y, 'Shape memory behaviors of crosslinked copolymers containing stearyl acrylate',*Macromol*. *Rapid Commun*., 1996, 17, 539*—*43.
- 16 He X, Oishi Y, Takahara A and Kajiyama T, 'Higher order structure and thermo-responsive properties of polymeric gel with crystalline side chains',*Polymer J*., 1996, 28(5), 452*—*7.
- 17 Sawhney A, Pathak C P and Hubbell J A, 'Bioerodible hydrogels based on photopolymerized poly(ethylene glycol)-*co*-poly(α-hydroxy acid) diacrylate macromers', *Macromolecules*, 1993, 26, 581*—*7.
- 18 McLoughlin R (RayChem, Ltd.), Method of making heat shrinkable articles, US Pat 4 425 174, 1984.
- 19 Sakurai K, Shirakawa Y, Kashiwagi T and Takahashi T, 'Crystal transformation of styrene-butadiene block copolymer', *Polymer*, 1992, 35(19), 4288*—*9.
- 20 Kim B K, Lee S Y and Xu M, 'Polyurethanes having shape memory effect',*Polymer*, 1996, 37, 5781*—*93.
- 21 Takahashi T, Hayashi N and Hayashi S, 'Structure and properties of shape-memory polyurethane block copolymers', *J*. *Appl*. *Polym*. *Sci*., 1996, 60, 1061*—*9.
- 22 Hayashi S (Mitsubihi Heavy Industries, Ltd.), Shape memory polyurethane elastomer molded article, US Pat 5 145 935, 1992.
- 23 Shirai Y and Hayashi S, Development of polymeric shape memory material, *Mitsubishi Tech*. *Bull*., 1988, 184.
- 24 Tobushi H, Hayashi S and Kojima S, 'Mechanical properties of shape memory polymer of polyurethane series', *JSME Int*. *J*., Series I, 1992, 35(3).
- 25 Ito K, Abe K, Li H L, Ujihira Y, Ishikawa N and Hayashi S, 'Variation of free

volume size and content of shape memory polymer *—* polyurethane *—* upon temperature', *J*. *Radioanalyt*. *Nucl*. *Chem*., 1996, 211(1), 53*—*60.

- 26 Tobushi H, Hayashi S, Ikai A and Hara H, 'Thermomechanical properties of shape memory polymers of polyurethane series and their applications', *J*. *Phys*. *IV*, *Coll*. *C12*, *Suppl*. *J*. *Phys*. *III*, 1996, 6, 377*—*84.
- 27 Li F, Hou J, Zhu W et al., 'Crystallinity and morphology of segmented polyurethanes with different soft-segment length', *J*.*Appl*.*Polymer Sci*., 1996, 62, 631*—*8.
- 28 Hayashi S, Kondo S and Giordano C, 'Properties and applications of polyurethaneseries shape memory polymer', *Antec 94*, 1994, 1998*—*2001.
- 29 Jeong H M, Lee J B, Lee S Y and Kim B K, 'Shape memory polyurethane containing mesogenic moiety', *J*. *Mater*. *Sci*., 2000, 35, 279*—*83.
- 30 Jeong H M, Lee S Y and Kim B K, 'Shape memory polyurethane containing amorphous reversible phase', *J*. *Mater*. *Sci*., 2000, 35, 1579*—*83.
- 31 Lendlein A, Grablowitz H and Langer R, in preparation.
- 32 Lendlein A, Schmidt A and Langer R 'AB-polymer networks based on oligo (-caprolactone) segments showing shape-memory properties', *Proc*. *Natl*. *Acad*. *Sci*. *USA*, 2001 98(3), 842*—*7.
- 33 Lendlein A, Neuenschwander P, Suter U W, 'Hydroxy-telechelic copolyesters with well defined sequence structure through ring-opening polymerization', *Macromol*. *Chem*. *Phys*., 2000, 201, 1067*—*76.

#### SEERAM RAMAKRISHNA

## **17.1 Introduction**

Use of textile structures in the medical field is not recent because sutures, which for centuries have been used for the closure of wounds or incisions, are fundamentally textile structures. The emergence of textiles apart from sutures, for various biomedical applications, became of real significance in the early 1950s. Nowadays they are commonly used in various biomedical applications, and are generally referred to as 'medical textiles'. Based on the application, they may be grouped into three broad categories (Table 17.1), namely healthcare and hygiene textiles, extracorporeal devices and surgical textiles.<sup>2</sup> In terms of volume of usage, surgical textiles are much smaller than healthcare and hygiene textiles. However, scientifically, surgical applications are far more challenging. In these applications, the textiles are expected to fulfil a number of requirements, including surface biocompatibility(chemical structure, topography, etc.), mechanical compatibility (elastic modulus, strength, stiffness, etc.), non-toxicity, durability in in vivo (human body environment) conditions and sterilizability. Due to recent advancements in textile engineering and biomedical research, the use of textiles in surgery is growing. They are routinely used to direct, supplement or replace the functions of living tissues of the human body. Soft tissue replacements or implants such as vascular grafts, skin grafts, hernia patches and artificial ligaments are made of textile structures.<sup>3-8</sup> Moreover, polymers reinforced with textiles, called polymer composite materials, are also considered in hard tissue replacements or implants such as dental posts, bone grafts, bone plates, joint replacements, spine rods, intervertebral discs and spine cages.<sup>9,10</sup> Table 17.2 is a partial list of some of the most common implant applications of textiles. Some implant applications are shown schematically in Fig. 17.1. As can be seen from Table 17.2, the implantable textiles are made from a variety of synthetic biomaterials, which are essentially non-living (avital) type. Although the synthetic biomaterials are fairly successful, the profound differences between them and the living tissues of the human body







17.1 Schematic illustration of various implants.

lead to problems such as infection, loosening, failure and finally rejection of implants. On the other hand, transplantation (transfer of a tissue from one body to another, or from one location in a body to another) is not always practical due to a shortage of donor tissue, and the risk of rejection and disease transfer. Hence, there is a need to develop biological substitutes (living or vital materials) to avoid these problems. The newly developed field of 'tissue engineering' combines mammalian cells and certain synthetic biodegradable





materials (materials that eventually disappear after being introduced into a living tissue or organism) to produce living (vital) synthetic tissue substitutes or replacement tissues.<sup>11-13</sup> It is envisaged that such tissue substitutes will merge seamlessly with the surrounding host tissues, eliminating problems associated with contemporary biomaterials and transplantation. Recognizing the potential of tissue engineering, researchers worldwide are harnessing techniques to produce tissue engineered skin,<sup>14</sup> cartilage,<sup>15</sup> nerve,<sup>16</sup> heart valve<sup>17</sup> and blood vessels.<sup>18,19</sup> It is also envisaged that, using tissue engineering techniques, it will eventually be possible to construct entire replacement organs such as the liver<sup>20</sup> and bladder.<sup>21</sup>



Table 17.3 Various scaffolds used in tissue engineering

\*PLAGA, PGLA, PLGA are co-polymers of polyglycolic acid (PGA) and polylactic acid (PLA).



17.2 Knitted fabric scaffold seeded with osteoblastic cells.

The basic concept of tissue engineering is to regenerate or grownewtissues and organs by culturing isolated cells from the tissue or organ of interest on porous biodegradable scaffolds or templates (Fig. 17.2). The scaffold acts as an extracellular matrix for cell adhesion and growth and/or regeneration. An important challenge is to pursuade the cells transplanted onto scaffolds to multiply and produce correct tissue matrices, which can take up and secrete protein, generate force and resistance, constrain permeability and exhibit other life processes. It has been recognized that the engineering of the scaffold is an important aspect, as it provides the optimal requirements for the survival, proliferation and differentiation of cells, and for the formation of tissue in in vitro or in vivo conditions depending on the intended application. Hence, there has been a multitude of research work carried out in the last decade to design and develop various types of optimum scaffolds for tissue engineering (Table 17.3). They may be broadly categorized into three groups based on the processing methods: (1) foams/sponges,<sup>22-27</sup> (2) three-dimensional (3D) printed substrates/templates<sup>28</sup> and (3) textile structures.<sup>29-39</sup> Textile structures form an important class of porous scaffolds used in tissue engineering.<sup>40-42</sup> This chapter reviews various textile scaffolds from the viewpoint of tissue engineering requirements and possible future developments.

# **17.2 Ideal scaffold system**

Making biological substitutes using the tissue engineering approach fundamentally encompasses several phases, namely: selection of scaffold material; fabrication of scaffold; preparation of scaffold; cell harvest from animal or human patient; cell seeding onto the scaffold; cell proliferation and differentiation; growth of mature tissue; surgical transplantation; and implant adaptation and assimilation. The following describes features of an ideal scaffold system. Specific requirements vary from one tissue to another.

- The material used for the scaffold should be biocompatible, not inducing an unfavourable tissue response in the host. The material should be ultra-pure, and easily and reliably reproducible into a variety of sizes and structures.
- In most applications, the support of a scaffold is needed only for a limited time. These temporary scaffolds cannot be removed easily because of tissue grown into the porous structure. Therefore, scaffolds have to be manufactured out of a biodegradable material in which the degradation rate has to be adjusted to match the rate of tissue formation. The scaffold should maintain its volume, structure and mechanical stability long enough to allowadequate formation of tissue inside the scaffold. However, none of the degradation products released should provoke inflammation or toxicity.
- ∑ Scaffolds must provide a reproducible microscopic and macroscopic structure with a high surface-area to volume ratio in order to allow a significant amount of cell*—*surface interaction. The scaffold processing method should not affect the biocompatibility or the desired degradation

behaviour of the material. It should also allowthe manufacture of scaffolds with controlled interconnected pore structure, pore size distribution and pore geometry, since these are important factors in tissue growth or regeneration.

- The average pore size and the macroscopic dimensions of a scaffold are important factors which are associated with cell proliferation and nutrition supply, from tissue culture media in vitro and through newly formed blood vessels in vivo, to cells and tissue. The pore size of such scaffolds should be sufficient to allow cells to grow in multiple layers in order to form a three-dimensional tissue. The optimal pore size may be highly variable, depending also on the intended application of the scaffold. For instance, it has been hypothesized that in orthotopic sites, pore sizes below  $400 \mu m$  lead to bone formation and pore sizes above  $400 \mu m$  lead to fibrous tissue ingrowth.<sup>45-48</sup> In addition to pore size, porosity, which more reflects the interconnectivity of the scaffold, is also important. High porosity maximizes the volume of tissue ingrowth and minimizes the amount of scaffold material used. It also facilitates transport of nutrients and cellular waste products. Another parameter is the pore morphology, which may be meaningful in favouring the ingrowth of certain cell types.<sup>49</sup>
- ∑ Scaffold surface chemistry should be suitable for cell attachment and cell proliferation.
- In certain tissue engineering applications, external electro-mechanical stimulations are often used to promote cell proliferation and tissue development. The scaffold should be able to retain its shape and structure under these electro-mechanical conditions.
- Further, the flexibility of such a scaffold should be close to that of its surrounding tissue so, once the vascularization starts, no extreme change in the mechanical properties between the host tissue and the scaffold can be experienced by the ingrowing tissue. Such forces could be harmful, not only for the vascularization process, but also because they could induce the formation of a different tissue from the desired one.

# **17.3 Scaffold materials**

As most cells are substrate dependent, the scaffold structure as well as the material has control over the cell adhesion and function. The various scaffold materials used in tissue engineering can be grouped into natural and synthetic materials. Collagen, chitin, starch, etc. are a fewexamples of natural materials (see Table 17.4). Natural materials are isolated from human, animal or plant tissues, which typically result in high costs and large batch-to-batch variations. In addition, these materials exhibit a very limited range of properties and are





often difficult to process. Synthetic materials are further classified into degradable<sup>23,50</sup> and non-degradable<sup>51</sup> types. The non-degradable materials, such as polyethylene, polyethyleneterephthalate (PET) and polytetrafluoroethylene (PTFE) may carry a risk of permanent tissue reaction.<sup>33</sup> On the other hand, synthetic biodegradable polymers, such as polyesters, polyanhydrides and polyorthoesters (see Table 17.4) offer control over structure and properties. They can be processed into various shapes and microstructures, such as desired surface area, porosity, pore size and pore size distribution. They can be tailored with degradation times ranging from several days up to years. Their surface properties can be altered to adapt to the biological requirements for cell adhesion, growth and function. Therefore, synthetic biodegradable polymers have been widely investigated in tissue engineering research.<sup>52–54</sup> From the literature (Tables 17.3 and 17.4) it is evident that biodegradable polyester-based materials dominate the tissue engineering applications compared to other biodegradable polymers. This is mainly due to the fact that polyesters of poly( $\alpha$ -hydroxy acids) are used successfully in various implant applications and have already been approved by the US Food and Drug Administration (FDA). Another factor could be the familiar processing and characteristics of these materials to many tissue engineering researchers. However, it is to be noted that the mechanical properties and degradation profiles of these polyesters are insufficient for certain applications. Moreover, certain copolymers may release toxic products during degradation. As tissue engineering applications continue to grow, it is important to find and develop alternative biodegradable polymers that meet the specific requirements of various tissues.

## **17.4 Textile scaffolds**

The need for scaffolds in tissue engineering is undisputed as cells cannot survive on their own and are substrate dependent. However, there is no universal scaffold that meets all the requirements of various tissues, as the optimum tissue engineering conditions vary from tissue to tissue. In other words, the targeted tissue dictates the optimum scaffold design. For example, for hard tissues, such as bone, scaffolds need to have high stiffness in order to maintain the space they are designated to provide the tissue with enough space for growth. If scaffolds are used as a temporary load-bearing device, they should be strong enough to maintain that load for the required time without showing any symptoms of failure. Used in combination with soft tissues, the flexibility and the stiffness of the scaffold have to be within the same order of magnitude as the surrounding tissues in order to prevent the scaffold from either breaking or collapsing and from stress shielding the adjacent tissues. The choice of scaffold for a tissue therefore depends on its characteristics. In addition to the mechanical properties, the optimum design of a scaffold for a specific tissue application requires consideration of microstructural, chemical and biological aspects. It is often difficult to isolate these aspects as they are interdependent and sometimes their effects are unknown. The following sections critically look into some of these aspects of different textile scaffolds.

## 17.4.1 Microstructural aspects

The microstructural aspects of scaffolds includes pore size, porosity, pore size distribution, pore connectivity and reproducibility of pores. These aspects are vital, as they provide the optimal spatial and nutritional conditions for the cells, and determine the successful integration of the natural tissue and the scaffold. For example, Hubbell and Langer<sup>37</sup> showed in their experiments that in animals, the size and alignment of pores in the scaffold greatly influence the amount and rate of vascular and connective tissue growth. Fibrovascular tissues require a pore size greater than  $500 \mu m$  for rapid vascularization, whereas the optimal porosity for bone bonding materials is considered to be between 70 and 200  $\mu$ m.<sup>55</sup> In another study,<sup>56</sup> osteoblasts cultured in calcium phosphate ceramic prefer a pore size of  $200 \mu m$ , and it has been proposed that this pore size possesses a curvature that optimizes the compression and tension of the cell's mechanoreceptors. However, there is concern that optimal pore size in ceramics may not generalize for all scaffold materials.<sup>57</sup> For example, when poly(lactic acid) was implanted in calvarial rat defects, pore sizes of 300–350 µm supported bone ingrowth while smaller sizes did not. Yet, in another study, osteoblasts showed no significant difference in proliferation or function when seeded on poly(lactic glycolic acid) foams with pore sizes of either  $150-300 \,\mu m$ ,  $300-500 \,\mu m$  or  $500-710 \,\mu m$ . The importance of determining optimum values for the specific cells or tissue cannot be underestimated. In another study related to skin tissue engineering, Nerem et al.<sup>18</sup> showed that the endothelial morphology depends on the pattern of the scaffold. The interconnectivity of pores determines the transport of nutrients and waste and thus influences the success of tissue engineering. The reproducibility of scaffolds is also very important as it determines the dimensional stability of the scaffold as well as the consistency of the tissue formation. Table 17.5 compares the various microstructural aspects of foams and textile structures. Owing to the processing techniques employed, in general, each batch of foam will have one particular of porosity. It is possible to tailor the porosity to a certain extent. However, within the same foam, organizing or grading the porosity in a particular fashion may be difficult to achieve with the current processing techniques. On the other hand, textile structures can be tailored to give the required porosity in terms of size, quantity and distribution pattern. For example, in a typical textile scaffold, three levels of porosity can be achieved. The arrangement of fibres in the yarn determines the accessible space for cells. The inter-fibre space (or groove between two adjacent fibres) may be considered as the first level of porosity. In our study<sup>58</sup> it was found that the fibroblasts preferentially organize themselves along the length of the fibres, grouping along the groove created by two adjacent fibres. Figure 17.3 shows SEM pictures of polyethylene terephthalate (PET) fibre yarn before and after seeding with fibroblasts. What is more interesting is that fibroblasts are capable of bridging fibres which are as far as  $40 \mu m$  apart (Fig. 17.4). The inter-fibre gap or first level of porosity in a textile scaffold can be controlled by changing the number of fibres in the yarn and also the yarn packing density. Further variations in porosity can be achieved by using twisted, untwisted, textured, untextured, continuous or spun yarns.

The gap or open space between the yarns (it is open space inside the loop in the case of knits) forms the second level of porosity. In the case of knitted scaffolds, the porosity can be varied selectively by changing the stitch density and the stitch pattern. In the case of braided scaffolds, porosity can be varied by controlling the bias angle of the interlacing yarns. In the case of woven scaffolds, it is possible to change the porosity by controlling the inter-yarn gaps through a beating action. In our preliminary study<sup>58</sup> involving the seeding of woven, braided and knitted scaffolds with hepatocytes, it was observed that cells attach preferentially at the inter-yarn gaps or pores in the case of woven and braided scaffolds, whereas they clump together on the ridges of curved yarns in the case of knitted scaffolds (Fig. 17.5). It may be noted that woven and braided scaffolds share similar surface topographies formed by the interlacing yarns. Knitted scaffolds, however, comprise curved yarns, which had a significant effect on the behaviour of hepatocytes. The same

#### Table 17.5 Microstructural aspects of scaffolds



Textile structures



17.3 PET fibre yarn (a) before and (b) after seeding with fibroblasts (Cos7 kidney cells from SV40-transformed African green monkey).

experiment was repeated with fibroblasts to investigate the effect of cell type. Unlike the hepatocytes, the fibroblasts were found to attach to the ridges of yarns irrespective of the scaffold type. The different behaviour of fibroblasts and hepatocytes may be due to their different cell sizes and shapes. It may be noted that the diameter of fibroblasts ranges from  $10 \mu m$  to  $20 \mu m$ , and they flatten out after attachment. The hepatocytes are larger with diameters in the range  $15 \mu m$  to  $30 \mu m$ , and they retain their spherical structure even after attachment to the scaffold.

Furthermore, a third kind of porosity can be introduced by subjecting the textile structures to secondary operations such as crimping, folding, rolling, stacking, etc. In other words, the flexibility of microstructural parameters is tremendous in the case of textile scaffolds.

Bowers et al.<sup>59</sup> investigated the effect of surface roughness. It has been reported that a higher percentage of osteoblast-like cells cultured on commercially pure Ti attached to rougher surfaces than to smooth surfaces. Another study using the same material showed higher osteocalcin content and ALPase activity on smooth, polished surfaces than on rough surfaces.<sup>60</sup> In our



17.4 Fibroblasts bridging adjacent PET fibres.

study<sup>58</sup> involving woven, braid and knitted scaffolds, it was observed that the fibroblasts prefer to attach to the ridges of scaffolds rather than the valleys. This may be due to the cell's attempt to minimize distortion to its cytoskeleton in response to the topography of the scaffold. Further systematic study is needed to fully understand the influence of scaffold topology on tissue engineering.

# 17.4.2 Mechanical aspects

Similar to the microstructural aspects, the mechanical aspects of scaffolds, such as structural stability, stiffness and strength, have considerable influence on the cellular activity. For example, in tissues like bone, cell shape is influenced by mechanical forces.<sup>11</sup> Cell shape modification takes place as a result of external forces including gravity, and also of internal physical forces. Cell shape modification also depends on the nature (constant or cyclic), type (uniaxial, biaxial, multiaxial, etc.) and magnitude of the mechanical stimulation. The mechanical stimulation also affects the release of soluble signalling factors and the deposition of extracellular matrix constituents. Researchers are



17.5 Hepatocytes (cells from Wistar rats) attached preferentially at (a) interyarn gaps in a woven scaffold and  $(b)$  ridges of curved yarn in a knitted scaffold.

making use of these observations in the case of bone tissue engineering. They are applying external mechanical stimulation to promote tissue formation. Therefore, in bone tissue engineering, the scaffolds are designed to withstand severe physiological loads.<sup>55</sup> In blood vessel applications, the scaffold needs to be strong enough to withstand physiologically relevant pulsatile pressures and at the same time match the compliance or elasticity values of a native blood vessel. The mechanical aspects of various scaffolds are compared in Table 17.6. Among the scaffolds, the woven fabrics are normally rigid and inflexible due to the tight interlacing of yarns. The next stiff and strong scaffold is the braid. Knits, non-woven and foams display the lower end of the mechanical properties. Of all the scaffolds, knits display considerable deformability and good compliance owing to their looped yarn arrangement. Hence, they are suitable for bladder and blood vessel tissue engineering applications. Researchers are using woven scaffolds for tissue engineering of bone and acetabular cups. It is to be noted that the mechanical behaviours of scaffolds can be varied significantly by controlling the various microstructural aspects stated earlier. In other words, both the microstructural and mechanical aspects are





interrelated and it is less meaningful to understand them individually. Further work is necessary to understand how the scaffolds behave in in vitro or in vivo environments, and how they contribute to the growth of tissue.

## 17.4.3 Other aspects

There is increasing evidence that scaffold surface chemistry influences cellular activity.<sup>61</sup> Boyan et al.<sup>113</sup> showed that osteoblast response varies with the material on which cells are cultured, and attributed this to differences in the surface chemistry, charge density and net polarity of the charge. Some variations have been attributed to the proteins present in the medium that adsorb onto the surface to different degrees or with different structural  $arrangements.  $62$  In one study, osteoblasts were cultured on glass modified$ with the RGD peptide or non-adhesive, scrambled sequence and in the presence or absence of BMP-7. $63$  The culture with a combination of RGD substrate and BMP-7 showed a substantial increase in mineralization in 21 days over all other combinations of treatments. Because of its role in both attachment and differentiation, RGD incorporation may contribute greatly to scaffold osteoinductivity and bone regeneration. Technologies for the incorporation of peptides on to the scaffold surfaces are being further perfected.

In our laboratory, a systematic study<sup>58</sup> was made involving unmodified polyethylene terephthalate (PET) textile scaffolds and YIGSR (Tyr*—*Ile*—*Gly*—*Ser*—*Arg) peptide conjugated PET textile scaffolds. Three types of scaffolds, namely woven, braided and knitted fabrics, were seeded with fibroblasts (Cos7 kidney cells from SV40-transformed African green monkey) and hepatocytes (cells from Wistar rats) separately. All three types of scaffolds indicated a 35% to 46% increase in the number of fibroblasts attached when conjugated with peptide bonds compared to the unmodified scaffolds. However, no appreciable change in the hepatocyte attachments was found with the peptide surface modification of scaffolds. This study clearly indicates that the cellular activity also depends on the source of cells (bone, liver, blood vessels, etc.), number of cell types (pure, co-cultured or mixed cell type cultures), species (e.g. rat, rabbit, chicken, human), sex and age (i.e. embryonic, neonatal or adult). Furthermore, it is generally believed that, depending on the characteristics of the cell culture and culture period used, different reactions may be expected. The current literature clearly indicates that a combination of various factors, such as scaffold material, structure, physical, chemical, mechanical, and biological properties, cell types, in vitro or in vivo conditions, etc., determines the success of tissue engineering.

## **17.5 Conclusions**

Scaffolds play a central role in tissue engineering. Textile structures are particularly attractive to tissue engineering because of their ability to tailor a broad spectrum of scaffolds with a wide range of properties. Preliminary studies clearly demonstrate the suitability of textile scaffolds for tissue engineering purposes. There is no universal scaffold that meets the requirements of the various tissues of the human body. Further systematic study is necessary to design an optimal scaffold for each tissue application.

# **Acknowledgements**

The author wishes to thank Professor Kam W. Leong, Johns Hopkins University, USA, and Dr J. Mayer, Swiss Federal Institute of Technology, Switzerland for their valuable suggestions and discussions. The author also appreciates the support of Dr Hanry Yu and contributions of Miss Wee Su-Leng Serene, National University of Singapore, in preparing this chapter.

# **References**

- 1 Planck H, General aspects in the use of medical textiles for implantation. In *Medical Textiles for Implantation*, ed. H Planck, M Dauner and M Renardy, Springer-Verlag, Heidelberg, Germany, 1990, 1*—*16.
- 2 Adanur S, *Wellington Sears Handbook of IndustrialTextiles*. Technomic Publishing Co. Inc., USA, 1995.
- 3 Arnoczky S P, Torzilli PA et al., 'Biologic fixation of ligament prostheses and augmentations: An evaluation of bone in-growth in dog', *Am*. *J*. *Sports Med*., 1988, 16(2), 106*—*12.
- 4 Berry J L, Berg W S et al., 'Evaluation of dacron covered and plain bovine xenografts as replacements for the anterior cruciate ligament', *Clin*. *Orthop*., 1988, 236, 270*—*8.
- 5 Marios Y, Roy R et al, 'Histopathological and immunological investigations of synthetic fibers and structures used in three prosthetic anterior cruciate ligaments: in vivo study in the rat', *Biomaterials*, 1993, 14(4), 255*—*62.
- 6 Pietrucha K, 'Newcollagen implant as dural substitute', *Biomaterials*, 1991, 12(3), 320*—*3.
- 7 Molina J E, Edwards J E, Bianco R W, Clack R W, Lang G and Molina J R, 'Composite and plain tubular synthetic graft conduits in right ventricle-pulmonary artery position: fate in growing limbs', *J*. *Thorac*. *Cardiovasc*. *Surg*., 1995, 110(2), 427*—*35.
- 8 Menger M D, Hammersen F et al., 'In vivo assessment of neovascularization and incorporation of prosthetic vascular biografts', *Thorac*. *Cardiovasc*. *Surg*., 1992, 40(1), 19*—*25.
- 9 Ramakrishna S, Ramaswamy S, Teoh S H, Hastings G W and Tan C T,

'Application of textiles and textile composites concepts for biomaterials development', *Int*. *Conf*. *New Textiles for Composites*, *TEXCOMP 3 Conference Series*, Aachen, Germany, 1996, 27/1*—*27/27.

- 10 Ramakrishna S, Mayer J, Wintermantel E and Leong K W, 'Biomedical applications of polymer composite materials: a review', *Composites Science and Technology* (in press).
- 11 Langer R and Vacanti J, 'Tissue engineering', *Science*, 1993, 260, 920*—*6.
- 12 Peppas N A and Langer R, 'Newchallenges in biomaterials', *Science*, 1994, 263, 1715*—*20.
- 13 Langer R and Vacanti J, 'Artificial organs', *Sci*. *Amer*., 1995, September, 100*—*3.
- 14 Naughton G K, Bartel R and Mansbridge J, 'Synthetic biodegradable polymer scaffolds'. In *Synthetic Biodegradable Polymer Scaffolds*, ed. A Ataala, D J Mooney, J P Vacanti and R Langer, Birkhauser, Boston, USA, 1997, 121*—*47.
- 15 Cao Y, Ibarra C and Vacanti J P, 'Tissue engineering of cartilage and bone'. In *Synthetic Biodegradable Polymer Scaffolds*, ed. A Ataala, D J Mooney, J P Vacanti and R Langer, Birkhauser, Boston, USA, 1997, 199*—*214.
- 16 Dunn R L, 'Clinical applications and update on the poly( $\alpha$ -hydroxy acids)'. In *Biomedical Applications of Synthetic Biodegradable Polymers*, ed. J O Hollinger, CRC Press Inc., USA, 1995, 17*—*31.
- 17 Shinoka T and Mayer J E, 'Newfrontiers in tissue engineering: tissue engineered heart valves'. In *Synthetic Biodegradable Polymer Scaffolds*, ed. A Ataala, D J Mooney, J P Vacanti and R Langer, Birkhauser, Boston, USA, 1997, 188*—*98.
- 18 Nerem R M, Braddon L G, Seliktar D and Ziegler T, 'Tissue engineering and the vascular system'. In *Synthetic Biodegradable Polymer Scaffolds*, ed. A Ataala, D J Mooney, J P Vacanti and R Langer, Birkhauser, Boston, USA, 1997, 165*—*85.
- 19 Weinberg C B, O'Neil K D, Carr R M, Cavallaro J F, Ekstein B A, Kemp P D and Rosenberg M, 'Matric engineering: remodeling of dense fibrillar collagen vascular grafts in vivo'. In *Tissue Engineering*, *Current Perspectives*, ed. E Bell, Birkhauser, Boston, USA, 1993, 190*—*8.
- 20 Lee H and Vacanti J P, 'Tissue engineering of liver'. In *Synthetic Biodegradable Polymer Scaffolds*, ed. A Ataala, D J Mooney, J P Vacanti and R Langer, Birkhauser, Boston, USA, 1997, 235*—*51.
- 21 Atala A, 'Tissue engineering in the genitourinary system'. In *Synthetic Biodegradable Polymer Scaffolds*, ed. A Ataala, D J Mooney, J P Vacanti and R Langer, Birkhauser Boston, USA, 1997, 149*—*64.
- 22 Dagalakis N, Flink J, Stasikelis P, Burke J F and Yannas I V, 'Design of artificial skin. Part III. Control of pore structure', *J*. *Biomed*. *Mater*. *Res*., 1980, 14, 107*—*31.
- 23 Mikos A G, Thorsen A J, Czerwonka L A, Bao Y and Langer R, 'Preparation and characterization of poly(L-lactic acid) foams', *Polymer*, 1994, 35, 1068-77.
- 24 Thomson, R C, Yaszemski M J, Powers J M and Mikos A G, 'Fabrication of biodegradable polymer scaffolds to engineer trabecular bone', *J*. *Biomater*. *Sci*., *Polymer Edition*, 1995, 7, 23*—*38.
- 25 Lo H, Ponticiello M S and Leong K W, 'Fabrication of controlled release biodegradable foams by phase separation', *Tissue Eng*., 1995, 1, 15*—*28.
- 26 Mooney D J, Baldwin D F, Suh N P, Vacanti J P and Langer R, 'Novel approach to fabricate porous sponges of poly(D,L-lactic-*co*-glycolic acid) without the use of organic solvents', *Biomaterials*, 1996, 17, 1417*—*22.
- 27 Widmer M S, Evans G R D, Brandt K, Savel T, Patrik C W and Mikos A G, 'Porous biodegradable polymer scaffolds for nerve regeneration', *Proc*. *1997 Summer Bioengineering Conference*, Volume 35, ed. K B Chandran, R Vanderby Jr and M S Hefzy, The American Society for Mechanical Engineers, NewYork, 1997, 353*—*4.
- 28 Wu B M, Borland S W, Giordano R A, Cima L G, Sachs E M and Cima M J, 'Solid free-form fabrication of drug delivery devices', *J*. *Controlled Release*, 1996, 40, 77*—*87.
- 29 Katz A R and Turner R, 'Evaluation of tensile and absorption properties of polyglycolic acid sutures', *Surg*. *Gynecol*. *Obstet*., 1970, 131, 701*—*16.
- 30 Frazza E J and Schmitt E E, 'A newabsorbable suture', *J*. *Biomed*. *Mater*. *Res*. *Symp*., 1971, 1, 43*—*58.
- 31 Reed A M and Gilding D K, 'Biodegradable polymers for use in surgery  poly(glycolic)/poly(lactic acid) homo and co-polymers: 1',*Polymer*, 1981, 22, 505*—*9.
- 32 Reed A M and Gilding D K, 'Biodegradable polymers for use in surgery  poly(glycolic)/poly(lactic acid) homo and copolymers: 2. In vitro degradation', *Polymer*, 1981, 22, 494*—*8.
- 33 Cima L G, Vacanti J P, Vacanti C, Ingber D, Mooney D and Langer R, 'Tissue engineering by cell transplantation using degradable polymer substrates', *J*. *Biomed*. *Eng*., 1991, 113, 143*—*51.
- 34 Mikos A G, Bao Y, Cima L G, Ingber D E, Vacanti J P and Langer R, 'Preparation of poly(glycolic acid) bonded fiber structures for cell attachment and transplantation', *J*. *Biomed*. *Mater*. *Res*., 1993, 27, 183*—*9.
- 35 Shalaby S W and Johnson R A, 'Synthetic absorbable polyesters'. In *Biomedical Polymers*: *Designed*-*to*-*Degrade Systems*, ed. S W Shalaby, Carl Hanser Verlag, New York, USA, 1994.
- 36 Freed L E, Vunjak-Novakovic G, Biron R J et al., 'Biodegradable polymer scaffolds for tissue engineering', *Bio Technology*, 1994, 12, 689*—*93.
- 37 Hubbell J A and Langer R, 'Tissue engineering', *C*&*EN*, 1995, March 13, 42*—*54.
- 38 Piskin E, 'Biomaterials in different forms for tissue engineering: an overview'. In *Porous Materials for Tissue Engineering*, ed. D M Liu and V Dixit, Trans Tech Publications, Switzerland, Materials Science Forum, 1997, 250, 1*—*14.
- 39 Dauner M, 'Textile scaffolds for biohybrid organs', *Proc*. *Techtextil Symposium*: *Health and Protective Textiles*, France, 1998, 2, 67*—*72.
- 40 Mayer J, Karamuk E, Bruinink A, Wintermantel E and Ramakrishna S, 'Structural and mechanical aspects of textile scaffold systems for tissue engineering', *9th Int. Conf. Biomedical Engineering*, Singapore, 1997, 617*—*20.
- 41 Mayer J, Karamuk E, Bruinink A, Wintermantel E and Ramakrishna S, 'Textile scaffolding for tissue engineering: influence of structural deformation in the microscopic range', *Proc*. *Topical Conference Int*. *Conf*. *Biomaterials*, *Carriers for Drug Delivery*, *and Scaffolds for Tissue Engineering*, Los Angeles, USA, 1997, 96*—*8.
- 42 Leong K W and Ramakrishna S, 'Scaffold engineering', *Ann*. *Rev*. *Biomed*. *Eng*. (in press).
- 43 Widmer M S and Mikos A G, 'Fabrication of biodegradable polymer scaffolds for tissue engineering'. In *Frontiers in Tissue Engineering*, ed. C W Patrick, A G Mikos and L V Mcintire, Pergamon Press, USA, 1998, 107*—*20.
- 44 Chaignaud B E, Langer R and Vacanti J P, 'The history of tissue engineering using synthetic biodegradable polymer scaffolds and cells'. In *Synthetic Biodegradable*

*Polymer Scaffolds*, ed. A Ataala, D J Mooney, J P Vacanti and R Langer, Birkhauser, Boston, USA, 1997, 1*—*14.

- 45 Ducheyne P, 'Success of prosthetic devices fixed by ingrowth or surface interaction', *Acta Orthop*. *Belg*., 1985, 51, 144*—*61.
- 46 Schliephake H, Neukam F W and Klosa D, 'Influence of pore dimensions on bone ingrowth into hydroxyapatite blocks used as bone graft substitutes: a histometric study', *Int*. *J*. *Oral*. *Maxillofac*. *Surg*., 1991, 20, 53*—*8.
- 47 Eggli P S, Muller W and Schenk R K, 'Porous hydroxyapatite and tricalcium phosphate cylinders with two different pore size ranges implanted in cancellous bone of rabbits: a comparative histomorphometric and histologic study of bony ingrowth and implant substitution', *Clin*. *Orthop*. *Rel*. *Res*., 1988, 232, 127*—*38.
- 48 Collier J P, Mayor M B, Chae J C, Surprenant V A, Surprenant H P and Dauphinais L A, 'Macroscopic and microscopic evidence of prosthetic fixation with porous-coated materials', *Clin*. *Orthop*., 1988, 235, 173*—*80.
- 49 Kadiyala S, Lo H and Leong K W, 'Formation of highly porous polymeric foams with controlled release capability'. In *Tissue Engineering Methods and Protocols*, ed. J R Morgan and M L Yarmush, Humana Press, USA, 1999, 57*—*65.
- 50 Ma P X and Langer R, 'Degradation, structure and properties of fibrous nonwoven poly(glycolic acid) scaffolds for tissue engineering'. In *Proc*. *of MRS Symposium* Polymers in Medicine and Pharmacy, ed. A G Mikos, K W Leong, M L Radomsky, J A Tamada andM J Yaszemki,Materials Research Society, USA, 1995, 394, 99*—*104.
- 51 Pongor P, Betts J, Muckle D and Bentley G, 'Woven carbon surface replacement in the knee: independent clinical review', *Biomaterials*, 1992, 13, 1070*—*6.
- 52 Ma P X and Langer R, 'Fabrication of biodegradable polymer foams for cell transplantation and tissue engineering'. In *Tissue Engineering Methods and Protocols*, ed. J R Morgan and M L Yarmush, Humana Press, USA, Methods in Molecular Medicine, 1999, 18, 47*—*56.
- 53 Wong W H and Mooney D J, 'Synthesis and properties of biodegradable polymers used as synthetic matrices for tissue engineering'. In *Synthetic Biodegradable Polymer Scaffolds*, ed. A Atala, D J Mooney, J P Vacanti and R Langer, Birkhauser, Boston, USA, 1997, 51*—*82.
- 54 Leong K W, 'Chemical and mechanical considerations of biodegradable polymers for orthopaedic applications'. In *Biodegradable Implants in Fracture Fixation*, ed. K S Leung, L K Hung and P C Leung, World Scientific Publishing Co. Pte. Ltd., Singapore, 1994, 45*—*56.
- 55 Wintermantel E, Bruinink A, Eckert C L, Ruffieux K, Petitmermet M and Mayer J, 'Tissue engineering supported with structured biocompatible materials: goals and achievements'. In *Materials in Medicine*, ed. M O Speidel and P J Uggowitzer, vdf Hochschulverlag AG an der ETH Zurich, 1998, 1*—*136.
- 56 Dennis J E, Haynesworth S E, Young R G and Caplan A I, 'Osteogenesis in marrow derived mesenchymal cell porous ceramic composites transplanted subcutaneously: effect of fibronectin and lamin on cell retention and rate of osteogenic expression', *Cell Transpl*., 1992, 1, 23*—*32.
- 57 Robinson B, Hollinger J O, Szachowicz E and Brekke J, 'Calvarial bone repair with porous D,L-polylactide', *Otolaryngol*. *Head Neck Surg*., 1995, 112, 707*—*13.
- 58 Wee S S, 'Development of fibrous scaffolds for liver tissue engineering', *B*. *Eng*. *Dissertation*, National University of Singapore, Singapore, 2000.
- 59 Bowers K T, Keller J C, Randolph B A, Wick D G and Michaels C M, 'Optimization of surface micromorphology for enhanced osteoblast responses in vitro', *Int*. *J*. *Oral Maxillofac*. *Imp*., 1992, 7, 302*—*10.
- 60 Stanford C M, Keller J C and Solursh M, 'Bone cell expression on titanium surfaces altered by sterilization treatments', *J*. *Dent*. *Res*., 1994, 73, 1061*—*71.
- 61 Bostrom R D and Mikos A G, 'Tissue engineering of bone'. In *Synthetic Biodegradable Polymer Scaffolds*, ed. A Ataala, D J Mooney, J P Vacanti and R Langer, Birkhauser, Boston, USA, 1997, 215*—*34.
- 62 Kadiyala S, Lo H and Leong K W, 'Biodegradable polymers as synthetic bone grafts'. In *Bone Formation and Repair*, ed. C T Brighton, G Freidlaender and J M Lane, American Academy of Orthopedic Surgeons, USA, 1994, 317*—*24.
- 63 Norde W, 'The behavior of proteins at interfaces, with special attention to the role of the structure stability of the protein molecule', *Clin*. *Mater*., 1992, 11, 85*—*91.
- 64 Dee K C, Rueger D C, Anderson T T and Bizios R, 'Conditions which promote mineralization at the bone-implant interface: A model in vitro study', *Biomaterials*, 1996, 17, 209*—*15.
- 65 Vacanti C A, Kim W S and Mooney D, 'Tissue engineered composites of bone and cartilage using synthetic polymers seeded with two cell types', *Orthopaed*. *Trans*., 1993, 18, 276.
- 66 Kim W S, Vacanti J P, Cima L et al., 'Cartilage engineered in predetermined shapes employing cell transplantation on synthetic biodegradable polymers', *Plast*. *Reconstr*. *Surg*., 1994, 94, 233*—*7.
- 67 Freed L E and Vunjak-Novakovic G, 'Tissue engineering of cartilage'. In *The Biomedical Engineering Handbook*, ed. J D Bronzino, CRC Press, Boca Raton, 1995, 1788*—*803.
- 68 Laurencin C T, Ambrosio A M A, Borden M D and Cooper Jr J A, 'Tissue engineering: orthopedic applications', *Ann*. *Rev*. *Biomed*. *Eng*., 1999, 1, 19*—*46.
- 69 Laurencin C T, Ko F K, Borden M D, Cooper Jr J A, Li W J and Attawia M A, 'Fiber based tissue engineered scaffolds for musculoskeletal applications: *in vitro* cellular response'. In *Biomedical Materials — Drug Delivery*, *Implants and Tissue Engineering*, ed. T Neenan, M Marcolongo and R F Valentini, Materials Research Society, Warrendale, USA, 1999, 550, 127*—*35.
- 70 GottlowJ, 'Guided tissue regeneration using bioresorbable and non-resorbable devices: initial healing and long term results', *J*. *Periodontol*., 1993, 64, 1157.
- 71 Cao Y, Vacanti J P, Ma P X et al., 'Tissue engineering of tendon', *Proc*. *Mat*. *Res*. *Soc*. *Symp*., 1995, 394, 83*—*9.
- 72 Bellincampi L D, Closkey R F, Prasad R, Zawadsky J P and Dunn M G, 'Viability of fibroblast-seeded ligament analogs after autogenous implantation', *J*. *Orthop*. *Res*., 1998, 16, 414*—*20.
- 73 Kim S S, Utsunomiya H, Koski J A et al., 'Survival and function of hepatocytes on a novel three-dimensional synthetic biodegradable polymer scaffold with an intrinsic network of channels', *Ann*. *Surg*., 1998, 228(1), 8*—*13.
- 74 Chamberlain L J and Yannas I V, 'Preparation of collagen*—*glycosaminoglycan copolymers for tissue engineering'. In *Tissue Engineering Methods and Protocols*, ed. J R Morgan and M L Yarmush, Humana Press, USA, Methods in Molecular Medicine, 1999, 18, 3*—*17.
- 75 Tountas C P, Bergman R A, Lewis T W, Stone H E, Pyrek J D and Mendenhall H V,

'A comparison of peripheral nerve repair using an absorbable tubalization device and conventional sutures in primates', *J*. *Appl*. *Biomat*., 1993, 4, 261.

- 76 Maquet V and Jerome R, 'Design of macroporous biodegradable polymer scaffolds for cell transplanatation'. In *Porous Materials for Tissue Engineering*, ed. D M Liu and V Dixit, Trans Tech Publications, Switzerland, Materials Science Forum, 1997, 250, 15*—*42.
- 77 Atala A, Cima L G, Kim W et al., 'Injectable alginate seeded with chrondrocytes as a potential treatment for vesicoureteral reflux', *J*. *Urol*., 1993, 150, 745*—*7.
- 78 Atala A, Kim W, Paige K T, Vacanti C A and Retik A B, 'Endoscopic treatment of vesicoureteral reflux with a chrondrocyte-alginate suspension', *J*. *Urol*., 1994, 152, 641*—*3.
- 79 Kung I M, Wang F F, Chang Y C and Wang Y J, 'Surface modifications of  $alginate/poly(L-lysine)$  microcapsular membrane with poly(ethylene glycol) and poly(vinyl alcohol)', *Biomaterials*, 1995, 16, 649*—*55.
- 80 Polk A, Amsden B, De Yao K, Peng T and Goosen M F, 'Controlled release of albumin from chitosan-alginate microcapsules', *J*. *Pharm*. *Sci*., 1994, 83, 178*—*85.
- 81 Pachence J M, 'Collagen-based devices for soft tissue repair', *J*.*Biomed*.*Mater*. *Res*., 1996, 33, 35*—*40.
- 82 Bell E, Rosenberg M, Kemp P et al., 'Recipes for reconstructing skin', *J*. *Biomech*. *Eng*., 1991, 113, 113*—*19.
- 83 Mooney D J and Rowley J A, 'Tissue engineering: integrating cells and materials to create functional tissue replacements'. In *Controlled Drug Delivery*: *Challenges and Strategies*, ed. K Park, American Chemical Society, USA, 1997, 333*—*46.
- 84 Krewson C E, Chung S W, Dai W and Saltzman W M, 'Cell aggregation and neurite growth in gels of extracellular matrix molecules', *Biotechnol*. *Bioeng*., 1994, 43, 555*—*62.
- 85 Yannas I V, 'Applications of ECM analogs in surgery', *J*. *Cell*. *Biochem*., 1994, 56, 188*—*91.
- 86 Hansbrough J F, Cooper M L, Cohen R et al., 'Evaluation of a biodegradable matrix containing cultured human fibroblasts as a dermal replacement beneath meshed skin graft on athymic mice', *Surgery*, 1992, 111, 438*—*46.
- 87 Mooney D J, Organ G M, Vacanti J P and Langer R, 'Design and fabrication of biodegradable polymer devices to engineer tubular tissues', *Cell Transplantation*, 1994, 3, 203*—*10.
- 88 Johnson L B, Aiken J, Mooney D et al., 'The mesentery as a laminated vascular bed for hepatocyte transplantation', *Cell Transplantation*, 1994, 3, 273*—*81.
- 89 Mooney D J, Park S, Kaufmann P, Sano K, McNamara K, Vacanti J P and Langer R, 'Biodegradable sponges for hepatocyte transplantation', *J*. *Biomed*. *Mater*. *Res*., 1995, 29, 959*—*65.
- 90 Zhang X et al., 'Biodegradable polymers for orthopedic applications', *Rev*. *Macromol*. *Chem*. *Phys*., 1993, C33, 81.
- 91 Gilding D K and Reed A M, 'Biodegradable polymers for use in surgery  polyglycolic/poly(lactic acid) homo- and copolymers', *Polymer*, 1979, 20, 1459*—*64.
- 92 Engelberg I and Kohn J, 'Physico-mechanical properties of degradable polymers used in medical applications: a comparative study',*Biomaterials*, 1991, 12, 292*—*304.
- 93 Cooper M L, Hansbrough J F, Speilvogel R L, Cohen R, Bartel R L and Naughton G, 'In vivo optimization of a living dermal substitute employing cultured human

fibroblasts on a biodegradable polyglycolic acid or polyglactic mesh',*Biomaterials*, 1991, 12, 243*—*8.

- 94 Kim I M and Vacanti J P, 'Tissue engineering'. In *The Biomedical Engineering Handbook*, ed. J D Bronzino, CRC Press, Boca Raton, USA, 1995.
- 95 Ma P X, Schloo B, Mooney D and Langer R, 'Development of biomechanical properties and morphogenesis of in vitro tissue engineered cartilage', *J*. *Biomed*. *Mater*. *Res*., 1995, 29, 1587*—*95.
- 96 Puelacher W C, Mooney D, Langer R, Upton J, Vacanti J P and Vacanti C A, 'Design of nasoseptal cartilage replacements synthesized from biodegradable polymers and chrondrocytes', *Biomaterials*, 1994, 15, 774*—*8.
- 97 Merrell J C, Russell R C and Zook E G, 'Polyglycolic acid tubing as a conduit for nerve regeneration', *Ann*. *Plast*. *Surg*., 1986, 17, 49*—*58.
- 98 Pham H N, Padilla J A, Nguyen K D and Rosen J M, 'Comparison of nerve repair techniques: sutures vs. avitene-polyglycolic acid tube', *J*. *Reconstr*. *Microsurg*., 1991, 1, 31*—*6.
- 99 Vert M, Christel P., Chalot F and Leray J, 'Bioresorbable plastic materials for bone surgery'. In *Macromolecular Biomaterials*, ed. G W Hastings and P Ducheyne, CRC Press, Boca Raton, USA, 1984.
- 100 Leong K W et al., 'Polyanhydrides'. In *Encycl*. *Polym*. *Sci*. *Eng*., ed. J I Kroschwitz, Wiley, New York, USA, 1989.
- 101 Heller J, 'Controlled drug release from poly(orthoester) *—* a surface eroding polymer', *J*. *Controlled Release*, 1985, 2, 167*—*77.
- 102 Daniels A U et al., 'Mechnical properties of biodegradable polymers and composites proposed for internal fixation of bone', *J*. *Appl*. *Biomater*., 1990, 1, 57.
- 103 Heller J and Daniels A U, 'Poly(orthoesters)'. In *Biomedical Polymers*: *Designed to Degrade Systems*, ed. SW Shalaby, Carl Hanser Verlag,Munich, Germany, 1994, 35.
- 104 Kohn J, 'Pseudopoly(aminoacids)'. In *Biodegradable Polymers as Drug Delivery Systems*, ed. M Chasin and R Langer, NewYork, USA, 1990, 195.
- 105 Pulapura S, Li C and Kohn J, 'Structure*—*property relationships for the design of polyiminocarbonates', *Biomaterials*, 1990, 11, 666.
- 106 Kadiyala S et al., 'Poly(phosphoesters) as bioabsorbable osteosynthetic materials'. In *Tissue Inducing Biomaterials*, ed. L Cima and E Ron, MRS Series, 1992252, 311.
- 107 Allcock H R, 'Phosphazene high polymers'. In *Comprehensive Polymer Science*, ed. G Allen, 4, Pergamon Press, New York, USA, 1989.
- 108 Allcock H R, Gebura M, Kwon S and Neenan T X, 'Amphiphilic polyphosphazenes as membrane materials: Influence of side group on radiation cross-linking', *Biomaterials*, 1988, 9, 500*—*8.
- 109 Allcock H R, Kwon S, Riding G H, Fitzpatrick R J and Bennett J L, 'Hydrophilic polyphosphazenes as hydrogels: radiation cross-linking and hydrogel characteristics of poly[bis(methyethoxythoxy)-phosphazene', *Biomaterials*, 1988, 9, 509*—*13.
- 110 Lora S, Carenza M, Palma G, Caliceti P, Battaglia P and Lora A, 'Biocompatible polyphosphazene by radiation-induced graft copolymerization and heparinization', *Biomaterials*, 1991, 12, 275*—*80.
- 111 Laurencin C T, Norman M E, Elgendy H M et al. 'Use of polyphosphazenes for skeletal tissue regeneration', *J*. *Biomed*. *Mater*. *Res*., 1993, 27, 963*—*73.
- 112 Razavi R, Khan Z, Haenerle C B and Beam D, 'Clinical applications of polyphosphazene-based resilient denture liner', *J*. *Prosthodontics*, 1993, 2, 224*—*7.
- 113 Scopelianos A G, 'Polyphosphzenes newbiomaterials'. In *Biomedical Polymers*: Designed-to-Degrade Systems, ed. S W Shalaby, Carl Hanser Verlag, New York, USA, 1994.
- 114 Boyan B D, Hummert T W, Dean D D and Schwartz Z, 'Role of material surfaces in regulating bone and cartilage cell response', *Biomaterials*, 1996, 17, 137*—*46.